

# ALUHD28

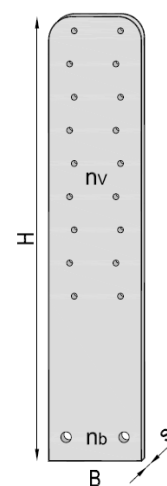
Traction plate for timber walls anchoring to AluBeam



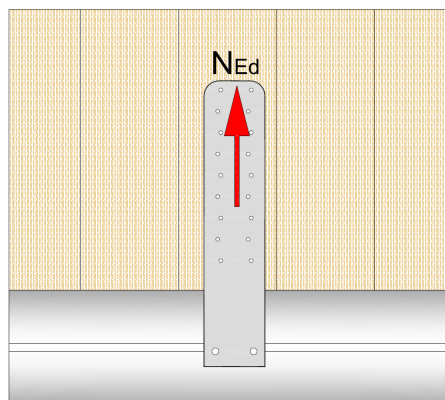
System components	Material
n.1 Plate ALUHD28	Aluminium EN AW-5754
n.1 guide with 2 threaded holes	Alluminio EN AW-6082
n.2 self-drilling bolts	Steel class 8.8, hot dip galvanizing

Use in service class 1 and 2

Code	B [mm]	H [mm]	s [mm]	nb f9	nv f5
ALUHD28	80	375	5	2	18



## FORCES



### DESIGN STRENGTH (METAL SIDE)

The design strength on the metal side for the Ultimate Limit State of ALUHD28, has been calculated following the assumptions below:

- Result of the design force through the geometrical gravity center of the holes for the wall fixing
- Material safety factors:
  - Aluminium ductile failure (EN 1999-1-1 §6.1.3)  $\gamma_{M1} = 1,10$
  - Aluminium brittle failure (EN 1999-1-1 §6.1.3)  $\gamma_{M2} = 1,25$
  - Bolts (EN 1993-1-8 §2.2)  $\gamma_{M2} = 1,25$

The plate strength verification must be done following the disequation below:


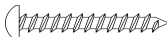
$$N_{Ed} \leq 28 \text{ kN}$$

where:

- $N_{Ed}$  is the traction force on the plate (ULS)

### TIMBER SIDE FIXING

d [mm]

Anker nail		4
Bolt for timber		4, 5

To calculate the strength of the fixing system of the timber side, the designer has to use Johansen formulas, basing on the one-shear-plane hypothesis (EN 1995-1-1, §8.2.3).

Advice for seismic verification: *in order to respect correctly the strengths hierarchy between ductile and brittle failure, our suggestion is to use a unitary safety factor ( $\gamma_M=1$ ) for the strength calculation of the connectors between the plate and the timber wall, as suggested by EC5 (tab. 2.3 - accidental combination) and to verify that the design strength of the connection on the metal side results greater than the timber side one.*